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TITLE OF THE INVENTION

OPTICAL TRANSMISSION DEVICE

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BACKGROUND OF THE INVENTIONField of the Invention

[0001] The present invention relates to communication devices and more specifically to optical transmission devices for providing two-way communication.

Description of the Related Art

[0002] Japanese Unexamined Patent Laid-Open No. 5-133716 discloses a conventional optical transmission device configured to perform two-way communication by using two communication devices that spatially separated from each other. Fig. 3 shows such an optical communication device A that communicates light beams LA as well as receives light beams LB from another communication device B (not shown).

[0003] In operation, a laser beam is emitted from a laser diode 101 and propagated as linearly polarized light through a lens group 102. Thereafter, it is reflected from a polarizing beam splitter 103, and then reflected by a variable-angle mirror 104a to the device B.

[0004] Similarly, the received light beam LB from device B is reflected by the variable-angle mirror 104a, through

the beam splitter 103 to branching element 105. A substantial portion of the light beam LB is transmitted through the branching element 105 to a photodetector 106 by a lens group 107. The other portion of light beam LB is reflected from the branching element 105 to a photodetector 108, which is a position detector, via a lens group 109.

[0005] In order to achieve the most efficient transmission and reception of light, an optical axis 112 on the beam splitter side, which corresponds to the common optical axis for transmission and reception, can be backwardly inclined so that the directions of the transmitting light beam LA and the received light beam LB form right angles with respect to each other.

[0006] For high-capacity communication, a small element having an effective light receiving area of less than 1 mm, such as an avalanche photodetector, must be used as the photodetector 106. And, the positions of the photodetector 106 and the position detecting photodetector 108 are aligned so that the light beam LB falls on the effective receiving area of the photodetector 106. The variable-angle mirror 104a is adjusted so that the optical axis of the light beam LB is at the center of the photodetector 108.

[0007] For efficient communication, the optical axis of the light beam LA is aligned with the center of the photodetector 108. A spot SP generated on the surface of

photodetector 108 by light beam LB, provides a misalignment information signal, which is transmitted to a mirror drive control unit 111 to generate a correction signal. Based on this signal, the angle of the variable-angle mirror 104a is adjusted to continuously align the optical axes of the light beams LA and LB.

[0008] The photodetector 108 generally employs a quadrant detector, which is divided into four elements 121 as shown in Fig. 4. The method for detecting a position using a photodetector has been described in e.g., Japanese Laid-open patent 2001-94513. Such a photodetector 108 is arranged so that the light receiving surface (plate) of the quadrant detector is generally located in a position defocused to a converging point of the lens group 109.

[0009] However, the optical transmission device, which transmits and receives light beams through the atmospheric air in the related art described above is affected by a phenomenon in which the transmitted light beam fluctuates due to microscopic fluctuations in the air.

[0010] Fig. 5 is an explanatory drawing showing modeled microscopic fluctuations, in which the distribution of strength of the transmitting light fluctuates in the atmosphere. The symbol W designates the width of light beam LA from device B. Since atmospheric air is inhomogeneous, the refractive index varies spatially and temporally. When

an air layer partially having a high refractive index exists in an optical pass of the transmission light LA, the portion of the high refractive index works as a convex lens, and thereby generates a light-concentrating effect and point W1, which is high in intensity, and point W2, which is low in intensity, are generated in the width W of the transmitting light beam LA at the position of the receiving device A.

Also, since the distribution of intensity varies temporally, point W2 appears to fluctuate within width W, a phenomena known as microscopic fluctuation. A disadvantage of the related art is that since the light receiving surface of the photodetector 108 is set at a position defocused from the converging point during microscopic fluctuations of the atmospheric air, the distribution of light intensity in spot SP becomes uneven.

In Fig. 5, the distribution of light intensity at the beam entrance of the device (the entrance pupil), is projected as shown. Consequently, the spot SP having an adequate area on the light receiving surface is as shown in Fig. 6.

[0011] As shown in Fig. 7, the spot SP having a diameter T, hatched portions P1 of high-intensity and portions P2 of low intensity are generated, and the center of light intensity PC, which differs from the center of luminous flux BC, is determined to be the optical axis. Therefore,

misalignment of the direction of the optical axis of the transmitting light beam LA occurs by an angle corresponding to an amount of misalignment S, and consequently, the transmitting light beam LA is deviated from the device B, which can cause interruptions in the communication system.

To solve the above-mentioned problems, it is preferable that photodetector 108 is arranged in a position adjacent to the converging point of the lens group 109 and the size of the spot SP is arranged so as to be less than the minimum resolution of the device. However, the light beam can intersect separation area 122 between each of the divided elements, and when the spot SP crosses over the light beam intersects separation area 122, the output from the photodetector 108 suddenly becomes low and is stopped in the worse case.

In such a case, although the optical axis actually exists on the photodetector 108 and the communication is normally and rightly being conducted, the system wrongly detects that the optical axis has been misaligned and moves the mirror 104a so as to align the optical axis. Thereby the optical axis existing on the photodetector 108 is shifted out of the correct range and the communication is terminated.

SUMMARY OF THE INVENTION

[0012] The present invention resolves one or more of the
aforementioned problems and provides a cost-effective
optical transmission device that allows stable communication
5 between two optical communication devices. Such stable
communication is achieved despite the presence of
microscopic fluctuations in the atmospheric air, which cause
optical axis misalignment resulting from uneven distribution
of light intensity in the received light beam. By employing
10 the present invention, such optical axis misalignment errors
are reduced or eliminated.

[0013] Accordingly, an optical transmission device
according to the present invention includes a transmission
unit for converting an electrical signal to an optical
15 signal, and a light receiving unit for converting the
received optical signal to an electrical signal.

A position detecting photodetector having a plurality of
light receiving units divided by parting lines for detecting
the direction of incidence of a luminous flux emitted from a
20 transmitting unit of an opposed partner device is provided,
and wherein the shape of a spot of a position detecting
light beam received by the position detecting photodetector
is linearly elongated on the position detecting
photodetector, and has a pattern, which satisfies relations:

$$L1/L2 > 3 \text{ and } L1 > 2^{1/2}D$$

where L1 represents the length of the major axis, L2 represents the length of the minor axis, and D represents the width of the parting lines. Further, the parting lines intersect with the spot shape at an angle.

5 [0014] As described above, in the optical transmission devices disposed opposite each other a predetermined distance apart and configured in such a manner that the device on the transmitting side converts an electrical signal to an optical signal and transmits it to the
10 receiving device and the device on the receiving side converts the received optical signal into an electric signal so that two-way information transmission is effected, the optical transmission device having an incidence direction detecting means for detecting the direction of incidence of
15 a luminous flux emitted from the opposed partner transmitting unit and directing a luminous flux emitted by itself toward the direction of incidence of the luminous flux, a cost-effective optical transmission device capable of performing stable communication is achieved by employing
20 a cross pattern filter having two or more cross patterns on the side of the partner transmitting unit with respect to the incidence direction detecting means, and arranging the cross pattern filter at the position where a cross pattern generated on the position detecting photodetector by the
25 cross pattern filter and parting lines for dividing the

position detecting photodetector do not lose the detection of the optical axis by the separation area between each of the divided even though the photodetector for detecting the optical axis is arranged in a position adjacent to the converging point of the lens for converging light received from the destination.

[0015] Further objects, features and advantages of the present invention will become apparent from the following description of the preferred embodiments (with reference to the attached drawings).

BRIEF DESCRIPTION OF THE DRAWINGS

[0016] Fig. 1 is a block diagram of an optical transmission device according to an embodiment.

[0017] Fig. 2 is a drawing showing a light receiving state on a position detecting photodetector according to the embodiment.

[0018] Fig. 3 is a block diagram of an optical transmission device in the related art.

[0019] Fig. 4 is a front view of a position detecting photodetector.

[0020] Fig. 5 is an explanatory drawing of modeled microscopic fluctuations of atmospheric air.

[0021] Fig. 6 is a drawing showing a light reception on

the position detecting photodetector in an optical transmission device in the related art.

[0022] Fig. 7 is a drawing of a beam spot on the position detecting photodetector in the optical transmission device in the related art.

[0023] Fig. 8 is a pattern diagram showing a diffraction pattern occurring due to a pinhole.

[0024] Fig. 9 is a pattern diagram showing a diffraction pattern according to Babinet's principle.

[0025] Fig. 10 is a diagram of striation patterns formed by utilizing Babinet's principle.

[0026] Fig. 11 is a drawing showing light convergence.

DESCRIPTION OF THE PREFERRED EMBODIMENT

First Embodiment

[0027] Fig. 1 is a schematic drawing showing an optical transmission device (device M) for providing stable communication with a device N (not shown) according to a first embodiment of the present invention. A laser beam, which is emitted from a laser diode 1, is propagated as linearly polarized light and is transmitted through a lens group 2 (with positive power). The beam is reflected from a boundary surface of a polarizing beam splitter 3, and is reflected by a variable-angle mirror 4a of an optical-axis

adjusting unit 4. It is then projected as transmitting light LA from device M to device N.

[0028] A received light beam LB is transmitted from the device N and is reflected by the variable-angle mirror 4a, and transmitted through the beam splitter 3 to a received light branching element 5. A substantial portion of the received light beam LB is transmitted through the beam branching element 5, and is converged onto a photodetector 6 by a lens group 7. The photodetector 6 acts as a real signal photodetector. The other portion of light beam LBb reflected from the beam branching element 5 is converged by a lens group 9 as a luminous flux through a cross pattern filter 13 for receipt by a photodetector 8.

[0029] Cross pattern filter 13 is a generic designation for an optical element generating radial striations from the luminous point of the image, and is also referred to as a cross filter, or a star filter. In operation, as shown in Fig. 8, a pinhole P is located on a shielding S between the lens and a focal point. Then, an optical image spreading from the center of the luminous flux passing through the pinhole P, which is the peak point, is observed at the focal point. The optical image spreads because the luminous flux does not converge to one point, but spreads due to diffraction when the luminous flux passes through the pinhole P.

However, according to Baninet's principle, as shown in Fig. 9, when shielding S is the same size as the pinhole P, and the shielding is formed on a transparent substrate B, and an inverted pattern formed by inverting the positive and negative (translucent and opaque) portions is arranged, an optical image identical to that formed by the pinhole, but opposite from the pinhole P in terms of positive and negative is generated due to a shadow. The difference is that a bright point image is formed by light which passes through the portion other than the shielding S. That is, when the shielding S is placed in the luminous flux converging to a point, blurring of the light results. Since this is a diffraction phenomenon, the smaller the shielding S, the larger the blur spreads, but the intensity of the blurred light is lowered. In contrast, the larger the shielding S, the smaller the width of the blur becomes, but the intensity of the blurred light increases. However, when the shielding S is excessively large, it is observed as a shadow.

Fig. 10 shows expansion of the shielding S in the direction perpendicular to the plane of the drawing. In this case, the blurred light becomes linear. The cross pattern filter is configured to generate a linear blur of light (referred to as striation) by employing linear shielding. For example, when shielding having lines

extending in two directions displaced by 90 degrees is provided, striations intersecting with an angle of 90 degrees are formed.

[0030] Various methods for arranging the shielding are apparent. For example, one example is a method of arranging narrow line-shaped shielding in a lattice-like pattern on a circular opening. Another example is a method of forming a lattice-like pattern on a transparent substrate by etching. Yet still, another example is a method of forming a lattice-like pattern by chrome. In the case where a lattice-like pattern is formed on the transparent substrate, the surface on which the pattern is formed may be either a plane surface or a curved surface. The same effects as the case where the shielding is provided may be obtained by forming a groove on the transparent substrate by patterning using replication, or by partly providing a diffusing surface thereon.

[0031] The difference in intensity of the light beam passing through the cross pattern filter 13 and detected by sensors provided on the position detecting photodetector 8 is transmitted to the mirror drive control unit 11 via the signal processing unit 10 as misalignment information. The mirror drive control unit 11 transmits an optical axis adjusting signal to the optical-axis adjusting unit 4 based on the misalignment information received. The optical-axis adjusting unit 4 changes the angle of the variable-angle

mirror 4a based on the optical axis adjusting signal to
adjust the optical axis. A cross pattern 21 formed by the
cross pattern filter 13 is disposed on the position
detection photodetector 8 so as not to overlap the parting
5 lines 122, which divide the sensor shown in Fig. 2.

Since the position detecting light beam received by the
position detecting photodetector 8 is converted into a cross
pattern having at least two striations, and is disposed so
as not to overlap the parting lines 122 dividing the sensor,
10 but to intersect therewith the luminous flux does not
completely enter the parting lines (blind zone) 122, and
hence the position detecting light beam cannot be lost from
sight without defocusing the converging point, even though
the position detection photodetector 8 is arranged in a
15 position adjacent to the converging point of the lens group
9. In addition, because most of the luminous flux entering
the beam entrance M of the device, which corresponds to the
entrance pupil, becomes the cross pattern 21 having high
light-gathering characteristics and an intensity
20 distribution more than $1/e^3$ in a peak of light amount,
generated on the position detection photodetector 8 by the
cross pattern filter 14, and hence is hardly affected by
microscopic fluctuations of the atmospheric air, if at all.
[0032] An exemplary spot shape is one that satisfies the
25 relational expressions:

$$L1/L2 > 3 \dots (1)$$

$$L1 > 2^{1/2} D \dots (2)$$

where L1 represents the length of the major axis of the spot, L2 represents the length of the minor axis of the spot, and D represents the width of the parting line of the position detecting photodetector.

[0033] The conditional expression (1) shows that the spot shape is linear, as shown by the reference numeral 21 in Fig. 2. When the value is smaller than the lower limit of the conditional expression (1), the cross pattern is subjected to microscopic fluctuations. Therefore, by setting the value larger than the lower limit and making the spot shape as close to the line as possible, microscopic fluctuation effects are reduced.

[0034] The conditional expression (2) defines the longitudinal direction of the major axis of the linear spot shape, which is the minimum length of the spot shape required for the position detecting photodetector to receive light. Preferably, the value of L1 is at least twice the value of D, when considering the accuracy of parts constituting the optical transmission device and the sensitivity of the position detecting photodetector.

[0035] It is also preferable to allow the position detecting photodetector to receive light so that the angle θ formed between the parting line and the spot length L1

satisfies the following expression, where α represents an angle formed between the parting lines:

$$\sin^{-1}(D/L1) < |\theta| < \alpha - \sin^{-1}(D/L1) \dots (3)$$

[0036] When the value deviates from the upper and lower limit in the conditional expression (3), even though the value satisfies the conditional expressions (1) and (2), all the light beam enters the parting lines (blind zone) and hence the position detecting light beam is lost from sight. Preferably, the angle θ formed between the parting line and the spot length $L1$ is on the order of half the angle α formed between the parting lines when considering the accuracy of parts constituting the optical transmission device and the sensitivity of the position detecting photodetector.

[0037] Since the exemplary size of the light receiving area of the position detecting photodetector is approximately 1 mm in diameter, and the width D of the parting line 122 is approximately 0.02 mm, assuming that the length $L1$ of the linear spot is 0.07 mm, the width $L2$ of the linear spot is 0.02 mm, the angle θ formed between the parting line and length $L1$ of the linear spot is 45 degrees, the angle α formed between the parting lines is 90 degrees,

$$L1/L2=3.5$$

$$L1=0.07=3.5D$$

The lower limit = 1.64 degrees and the upper limit =

88.36 degrees according to the conditional expression (3), and hence the conditional expressions (1) to (3) are satisfied.

[0038] Therefore, stable optical communication unaffected
5 by atmospheric microscopic fluctuations can be achieved.

And, the all the luminous flux is prevented from entering the parting lines 122 (blind zone). The light converging on the position detecting photodetector 8 may be as shown in Fig. 11, for example, and does not have to be a strictly
10 linear cross pattern as long as all the luminous flux does not enter into the parting lines 122.

[0039] While the present invention has been described with reference to what are presently considered to be the preferred embodiments, it is to be understood that the
15 invention is not limited to the disclosed embodiments. On the contrary, the invention is intended to cover various modifications and equivalent arrangements included within the spirit and scope of the appended claims. The scope of the following claims is to be accorded the broadest

20 interpretation so as to encompass all such modifications and equivalent structures and functions.